

# Mass Transfer

Fall 2024

Lecture #3

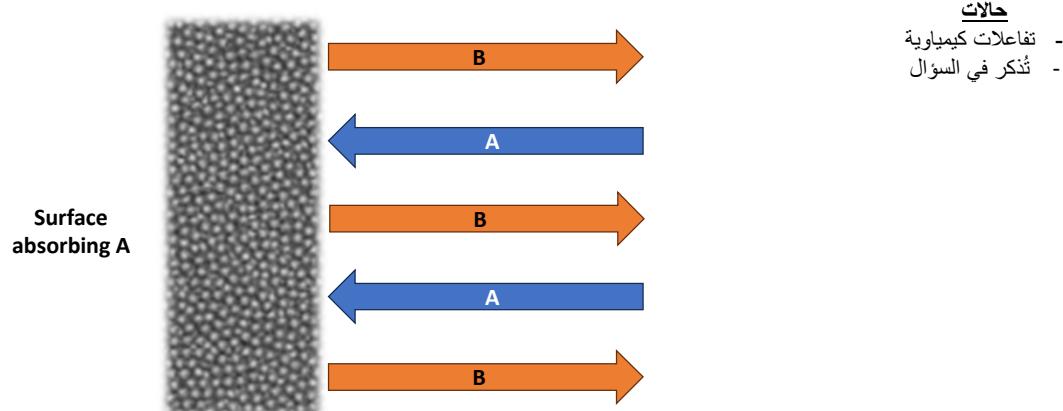
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## Molecular Diffusion

a) ii- Non-Equimolar- counter diffusion (NEMD)

Mass transfer rates of the two components are **not equal** but in **opposite directions**.



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## Molecular Diffusion

a) ii- Non-Equimolar- counter diffusion (NEMD)

**Example 5:** Drive the rate of diffusion of reaction of producing carbon dioxide from oxygen and charcoal particle.

**Solution**

$$\begin{array}{c} O_2 + 2Co \rightarrow 2Co_2 \\ \text{(A)} \qquad \qquad \text{(B)} \\ 2N_A = -N_B \quad \text{sub in (3)} \\ N_A = \frac{P_A}{P_t} (N_A + N_B) - \frac{D_{AB}}{R.T} \cdot \frac{dP_A}{dz} \quad \dots(3) \\ N_A = \frac{P_A}{P_t} (N_A + (-2N_A)) - \frac{D_{AB}}{R.T} \cdot \frac{dP_A}{dz} \\ N_A = \frac{P_A}{P_t} (-N_A) - \frac{D_{AB}}{R.T} \cdot \frac{dP_A}{dz} \\ N_A - \frac{P_A}{P_t} (-N_A) = -\frac{D_{AB}}{R.T} \cdot \frac{dP_A}{dz} \end{array}$$

$$\begin{aligned} N_A (1 + \frac{P_A}{P_t}) &= -\frac{D_{AB}}{R.T} \cdot \frac{dP_A}{dz} \\ N_A \cdot dZ &= -\frac{D_{AB}}{R.T} \cdot \frac{dP_A}{(1 + \frac{P_A}{P_t})} \\ N_A \cdot dZ &= -\frac{D_{AB} \cdot P_t}{R.T} \cdot \frac{dP_A}{(P_t + P_A)} \quad \text{By integration} \\ N_A \cdot \int_{Z_1}^{Z_2} dZ &= -\frac{D_{AB} \cdot P_t}{R.T} \cdot \int_{P_{A1}}^{P_{A2}} \frac{dP_A}{(P_t + P_A)} \\ N_A \cdot (Z_2 - Z_1) &= -\frac{D_{AB} \cdot P_t}{R.T} \cdot \ln \frac{(P_t + P_{A2})}{(P_t + P_{A1})} \\ N_A &= -\frac{D_{AB} \cdot P_t}{R.T} \cdot \frac{\ln \frac{(P_t + P_{A2})}{(P_t + P_{A1})}}{Z_2 - Z_1} \end{aligned}$$

لكل حالة يتم ايجاد معادلة من خلال التكامل



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## Molecular Diffusion

b) Diffusion of A in stagnant B, or unimolecular diffusion ( $N_B = 0$ )

Species A diffuses in stagnant non-diffusing B.

**Examples of Counter Diffusion:**

- Liquid evaporated to air
- Gas in air being absorbed into water (absorption column).

حالات انتشار مادة في وسط لاينشر  
 - برج امتصاص  
 - تبخير سائل  
 - ثذكر في السؤال

**Deriving the Case of A diffuses in stagnant non-diffusing B ( $N_B = 0$ ).**

$$N_A = \frac{P_A}{P_t} (N_A + N_B) - \frac{D_{AB}}{R.T} \cdot \frac{dP_A}{dz} ; \quad N_B = 0$$

$$N_A = \frac{P_A}{P_t} (N_A + 0) - \frac{D_{AB}}{R.T} \cdot \frac{dP_A}{dz} \Rightarrow N_A (1 - \frac{P_A}{P_t}) = -\frac{D_{AB}}{R.T} \cdot \frac{dP_A}{dz}$$

$$N_A (\frac{P_t - P_A}{P_t}) = -\frac{D_{AB}}{R.T} \cdot \frac{dP_A}{dz} \Rightarrow N_A \int_{Z_1}^{Z_2} dZ = -\frac{D_{AB} \cdot P_t}{R.T} \cdot \int_{P_{A1}}^{P_{A2}} \frac{dP_A}{(P_t - P_A)}$$



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## Molecular Diffusion

b) Diffusion of A in stagnant B. ( $N_B = 0$ )

$$N_A \int_{Z_1}^{Z_2} dZ = - \frac{D_{AB} \cdot P_t}{R \cdot T} \cdot \int_{P_{A1}}^{P_{A2}} \frac{dP_A}{(P_t - P_A)} \Rightarrow N_A (Z_2 - Z_1) = - \frac{D_{AB} \cdot P_t}{R \cdot T} \cdot (-\ln \frac{(P_t - P_{A2})}{(P_t - P_{A1})})$$

$$N_A = \frac{D_{AB} \cdot P_t}{R \cdot T} \cdot \frac{\ln \frac{(P_t - P_{A2})}{(P_t - P_{A1})}}{(Z_2 - Z_1)} ; \quad P_t - P_{A1} = P_{B1} ; \quad P_t - P_{A2} = P_{B2}$$

$$N_A = \frac{D_{AB} \cdot P_t}{R \cdot T} \cdot \frac{\ln \frac{P_{B2}}{P_{B1}}}{(Z_2 - Z_1)} ; \quad \text{Log mean partial pressure } P_{BM} = \frac{P_{B2} - P_{B1}}{\ln \frac{P_{B2}}{P_{B1}}}$$

$$N_A = \frac{D_{AB}}{R \cdot T} \left( \frac{P_t}{P_{BM}} \right) \cdot \frac{P_{B2} - P_{B1}}{(Z_2 - Z_1)} \Rightarrow N_A = - \frac{D_{AB}}{R \cdot T} \left( \frac{P_t}{P_{BM}} \right) \cdot \frac{P_{A2} - P_{A1}}{(Z_2 - Z_1)}$$



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**Example 6 :** Water in the bottom of a narrow metal tube is held at a constant temperature (293 K). The total pressure of dry air is  $1.0132 \times 10^5$  Pa at  $T = 293$  K. Water evaporates and diffuses through the air, the diffuses path is (0.15 m) long. **Calculate** the rate of evaporation at a steady state in  $Kmol/m^2 \cdot sec$ . Given that  $D_{AB} = 0.25 \times 10^{-4} m^2/sec$  and water vapor pressure at (20 °C) = 17.54 mm Hg.

### Solution

The water is diffused into the air but the air is not diffusing in the water, so ( $N_B = 0$ )

$$N_A = - \frac{D_{AB}}{R \cdot T} \left( \frac{P_t}{P_{BM}} \right) \cdot \frac{P_{A2} - P_{A1}}{Z_2 - Z_1}$$

$$P_{A1} = 17.54 \text{ mm Hg} = 17.54 \text{ mm Hg} * \frac{1 \text{ atm}}{760 \text{ mm Hg}} = 0.023 \text{ atm}$$

$$P_{A2} = 0 \text{ atm} \quad (\text{Pure air and large bulk volume})$$

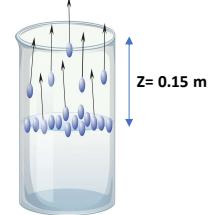
$$P_{B1} = P_t - P_{A1} = 1 - 0.023 = 0.977 \text{ atm}$$

$$P_{B2} = 1 \text{ atm}$$

$$P_{BM} = \frac{P_{B2} - P_{B1}}{\ln \frac{P_{B2}}{P_{B1}}} \Rightarrow P_{BM} = \frac{1 - 0.977}{\ln \frac{1}{0.977}} = 0.988 \text{ atm}$$

$$N_A = - \frac{0.25 \times 10^{-4}}{0.082 \times 293} \left( \frac{1}{0.988} \right) \cdot \frac{0 - 0.023}{0.15}$$

$$N_A = 1.64 \times 10^{-7} \text{ Kmol/m}^2 \cdot \text{sec}$$



*Note: in case ( $P_{B2} \approx P_{B1}$ ) then  $P_{BM}$  can be equal the average of  $P_{B2}$  &  $P_{B1}$*



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**Example 7:** Ammonia (A) diffuses through a stagnant layer of air (B), 1cm thick, at 25 °C and 1 atm total pressure. The partial pressures of ammonia on the two sides of the air layer are:  $P_{A0} = 0.9 \text{ atm}$  and  $P_{A1} = 0.1 \text{ atm}$  respectively. Air is non-diffusing. **Calculate:** a) The molar flux of ammonia in  $\text{Kmol}/\text{m}^2.\text{sec}$ . b) Molar and mass average velocity for each species at  $Z = 0$ . c) Plot the partial pressure distribution path.

Given that  $D_{AB} = 0.214 * 10^{-4} \text{ cm}^2/\text{sec}$

### Solution

a) For stagnant layer of air (B), ( $N_B = 0$ )

$$N_A = - \frac{D_{AB} \cdot P_t}{R \cdot T} \cdot \frac{\ln(P_t - P_{A1})}{(Z_1 - Z_0)}$$

$$P_{A0} = 0.9 \text{ atm} ; P_{A1} = 0.1 \text{ atm} ; P_t = 1 \text{ atm}$$

$$D_{AB} = 0.214 * 10^{-4} \text{ cm}^2/\text{sec}$$

$$N_A = - \frac{0.214 * 10^{-8} \left(\frac{\text{m}^2}{\text{sec}}\right) (1 \text{ atm})}{0.082 \left(\frac{\text{m}^3 \cdot \text{atm}}{\text{Kmol} \cdot \text{K}}\right) 298 \text{ K}} \cdot \frac{\ln\left(\frac{1-0.1}{1-0.9}\right)}{(0.01 \text{ m} - 0)}$$

$$N_A = 1.92 * 10^{-8} \text{ Kmol}/\text{m}^2.\text{sec}$$



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### Example 7:

### Solution

b) Molar and mass average velocity for each species

- Molar average velocity (U)

$$U = \frac{1}{c_t} (C_A \cdot u_A + C_B \cdot u_B) = \frac{1}{c_t} (N_A + N_B) = \frac{1}{c_t} (N_t)$$

for ( $N_B = 0$ )

$$U = \frac{1}{c_t} (N_A + 0) = \frac{N_A}{c_t} \quad \text{-----(*)}$$

$$C_t = \frac{P_t}{R \cdot T} = \frac{1 \text{ atm}}{0.082 \left(\frac{\text{m}^3 \cdot \text{atm}}{\text{Kmol} \cdot \text{K}}\right) 298 \text{ K}} = 0.041 \text{ Kmol/m}^3 \quad \text{sub in (*)}$$

$$U = \frac{1.92 * 10^{-8} \text{ Kmol}/\text{m}^2.\text{sec}}{0.041 \text{ Kmol}/\text{m}^3} = 4.6 * 10^{-7} \text{ m/sec}$$

$C_A$  varies along diffusion path, so  $u_A$  varies as well

$$\text{at } z = 0; P_{A0} = 0.9 \text{ atm} \Rightarrow y_{A0} = \frac{P_{A0}}{P_t} = \frac{0.9}{1} = 0.9$$

$$U = \frac{1}{c_t} (C_{A0} \cdot u_{A0} + C_{B0} \cdot u_{B0}) \quad ; \quad C_B \cdot u_B = N_B = 0$$

$$U = \frac{1}{c_t} \cdot (C_{A0} \cdot u_{A0}) = \frac{C_{A0}}{c_t} \cdot (u_{A0}) = y_{A0} \cdot (u_{A0})$$

$$u_{A0} = \frac{U}{y_{A0}} = \frac{4.6 * 10^{-7} \text{ m/sec}}{0.9} = 5.1 * 10^{-7} \text{ m/sec}$$

$$u_B = 0 \quad (\text{B stationary})$$



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**Example 7:****Solution**

b) Molar and mass average velocity for each species

- Mass average velocity ( $u$ )

$$u = \frac{1}{\rho_t} (\rho_A \cdot u_A + \rho_B \cdot u_B) ; \quad \rho_B \cdot u_B = 0$$

$$u = \frac{\rho_A \cdot u_A}{\rho_t} ; \quad \rho_i = \frac{P_i \cdot Mwt_i}{R \cdot T}$$

$$u = \frac{\frac{P_A \cdot Mwt_A}{R \cdot T} \cdot u_A}{\frac{P_t \cdot Mwt_t}{R \cdot T}} = \frac{P_A \cdot Mwt_A \cdot u_A}{P_t \cdot Mwt_t} = \frac{y_A \cdot Mwt_A \cdot u_A}{Mwt_t}$$

$$u = \frac{y_{A0} \cdot Mwt_A \cdot u_{A0}}{Mwt_t} \quad \text{---} (**)$$

At  $Z = 0$ 

$$y_A = 0.9 ; \quad y_B = 1 - y_A = 1 - 0.9 = 0.1$$

$$Mwt_t = y_A \cdot Mwt_A + y_B \cdot Mwt_B$$

$$Mwt_t = 0.9 * 17 + 0.1 * 29 = 18.2 \quad \text{sub in (**)}$$

$$u = \frac{0.9 * 17 * 5.1 * 10^{-7} \text{ m/sec}}{18.2} = 4.3 * 10^{-7} \text{ m/sec}$$


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**Example 7:****Solution**

c) Pressure distribution Plot

$$N_A = 1.92 * 10^{-8} \text{ Kmol/m}^2 \cdot \text{sec} = - \frac{D_{AB} \cdot P_t}{R \cdot T} \cdot \frac{\ln \left( \frac{(P_t - P_{A0})}{(P_t - P_{A1})} \right)}{(Z - Z_0)}$$

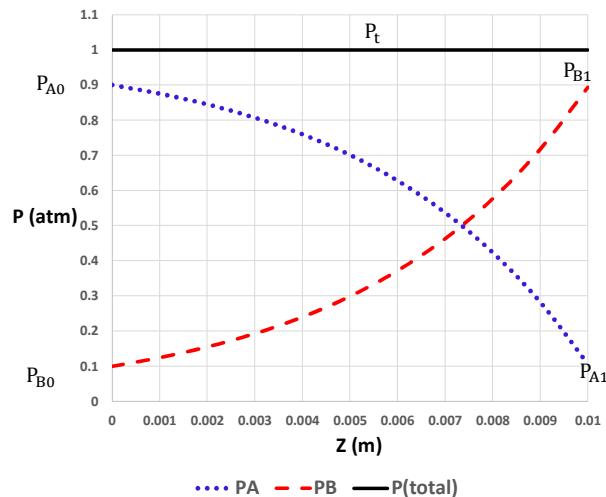
$$1.92 * 10^{-8} = - \frac{0.214 * 10^{-8} \left( \frac{\text{m}^2}{\text{sec}} \right) (1 \text{ atm})}{0.082 \left( \frac{\text{m}^3 \cdot \text{atm}}{\text{Kmol} \cdot \text{K}} \right) 298 \text{ K}} \cdot \frac{\ln \left( \frac{1 - P_A}{1 - 0.9} \right)}{(Z - 0)}$$

$$219 \text{ Z} = \ln \left( \frac{1 - P_A}{0.1} \right) \quad \text{by exponential both sides}$$

$$\exp(219 \text{ Z}) = \frac{(1 - P_A)}{0.1}$$

$$P_A = 1 - (0.1) \exp(219 \text{ Z})$$

$$P_B = (P_t - P_A)$$


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**HW 3:** Due date Saturday, October 26<sup>th</sup>

**Q1** Oxygen (A) diffuses through a stagnant layer of nitrogen (B) at 20°C and 1 atm total pressure. The diffusion path is 1 cm thick. The partial pressure of oxygen on one side of the layer is 0.8 atm, and on the other side, it is 0.2 atm. Nitrogen does not diffuse. Given the diffusivity of oxygen in nitrogen is  $D_{AB} = 0.18 \times 10^{-4} \text{ m}^2/\text{sec}$ , calculate:

1. The molar flux of oxygen.
2. The molar and mass average velocities for each species.

**Q2** Ammonia ( $NH_3$ ) diffuses through a stagnant layer of nitrogen ( $N_2$ ) at 300 K and 1 atm total pressure. The thickness of the stagnant nitrogen layer is  $L=0.01 \text{ m}$ . The partial pressure of ammonia at the surface ( $Z_0 = 0$ ) is  $P_{A0} = 0.8 \text{ atm}$ , and at the far side ( $Z=L$ ) it is  $P_{A1} = 0.2 \text{ atm}$ . The diffusion coefficient  $D_{AB} = 0.16 \times 10^{-4} \text{ m}^2/\text{sec}$ .

Find the partial pressure of ammonia at a distance  $Z=0.005 \text{ m}$  from the surface.



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