

Al-Mustaqbal University

Department (Power Mechanics Technologies Engineering)

Class (Four)

Subject (Air conditioning system) Lecturer (Qusay Rasheed Abd Al-amir)

1stterm – Lect. (outlet1)

The general procedure for use of Table 11-2 is as follows:

- 1. Determine the air-flow requirements and the room size.
- 2. Select the number, location, and type of diffuser to be used.
- 3. Determine the room characteristic length.
- 4. Select the recommended throw-to-length ratio from Table 11-2.
- 5. Calculate the throw.
- 6. Select the appropriate diffuser from catalog data such as those in Tables 11-3, 11-4, 11-5, or 11-6.
- 7. Make sure any other specifications are met (noise, total pressure, etc.).

Ex: The room shown in Figure (1) is part of a single-story office building located in the central United States. A perimeter air-distribution system is used. The air quantity required for the room is **250 cfm**. Select diffusers for the room based on cooling.

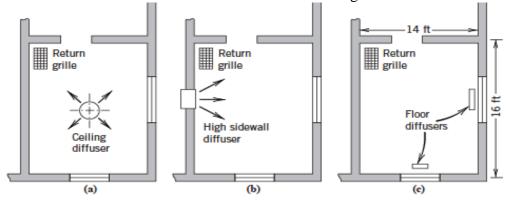


Figure 1 Plan view of a room showing location of different types of outlets.

Solution:

Diffusers of the type shown in **Table 11-3** should be used for this application.

A diffuser should be placed under each window in the floor near the wall (Figure c) because the room has two exposed walls. This will promote mixing with the warm air entering through the window. The total air quantity is **divided equally** between the two diffusers (250/2 = 125 cfm). If we assume that the room has an 8 ft ceiling and a room cooling load of 40 Btu/(hr-ft2), the room characteristic length is 8 ft (16/2).

Table 11-2 gives a throw-to-length ratio of 1.3 for a straight vane diffuser. Then

$$\frac{x50}{L} = 1.3 \rightarrow \frac{x50}{8} = 1.3 \rightarrow x50 = 10.4 \text{ ft} \text{ (throw=blow)}$$

From Table 11-3, $\underline{a} \ \underline{4} \times \underline{12} \ \underline{in}$ diffuser with $\underline{125} \ \underline{cfm}$ has a throw (blow), corrected for length, between

$$x50 = 13(\frac{3}{4}) = 9.7 \text{ ft} \text{ and } x50 = 17(\frac{3}{4}) = 12.7 \text{ ft}$$

because 125 cfm lies between 111 cfm and 139 cfm.

The NC is quite acceptable and is between $\underline{12}$ and $\underline{18}$, uncorrected for length. The total pressure required by the diffuser is between 0.036 and 0.057 in. wg and is about

$$\Delta P = (125/111)^2 \times (0.036) =$$
0.046 in. wg

An acceptable solution is listed as follows:

Size, in.	Capacity, cfm	Throw, ft	NC	ΔP_0 , in. wg
4×12	125	10.5	<15	0.046

The loss in total pressure for the diffuser is an important consideration. The value shown above would be acceptable for a light commercial system.

Table 11-1 Characteristic Room Length for Several Diffusers

Diffuser Type	Characteristic Length L
High sidewall grille	Distance to wall perpendicular to jet
Circular ceiling diffuser	Distance to closet wall or intersecting air jet
Sill grille	Length of room in direction of jet flow
Ceiling slot diffuser	Distance to wall or midplane between outlets
Light troffer diffusers	Distance to midplane between outlets plus distance from ceiling to top of occupied zone
Perforated, louvered ceiling diffusers	Distance to wall or midplane between outlets

Source: Reprinted by permission from ASHRAE Handbook, Fundamentals Volume, 1997.

Table 11-2 Air Diffusion Performance Index (ADPI) Selection Guide

	Room	x_{50}/L^a for		For ADPI	
Terminal	Load,	Maximum	Maximum	Greater	Range of
Device	Btu/hr-ft ²	ADPI	ADPI	Than	x_{50}/L^a
High sidewall	80 (252)	1.8	68	_	
grilles	60 (189)	1.8	72	70	1.5-2.2
	40 (126)	1.6	78	70	1.2 - 2.3
	20 (63)	1.5	85	80	1.0-1.9
Circular ceiling	80 (252)	0.8	76	70	0.7 - 1.3
diffusers	60 (189)	0.8	83	80	0.7 - 1.2
	40 (126)	0.8	88	80	0.5-1.5
	20 (63)	0.8	93	90	0.7 - 1.3
Sill grille,	80 (252)	1.7	61	60	1.5-1.7
Straight vanes	60 (189)	1.7	72	70	1.4-1.7
	40 (126)	1.3	86	80	1.2-1.8
	20 (63)	0.9	95	90	0.8 - 1.3
Sill grille,	80 (252)	0.7	94	90	0.6-1.5
Spread vanes	60 (189)	0.7	94	80	0.6 - 1.7
-	40 (126)	0.7	94	_	_
	20 (63)	0.7	94	_	_
Ceiling slot	80 (252)	0.3	85	80	0.3 - 0.7
diffusers	60 (189)	0.3	88	80	0.3 - 0.8
$(\text{for } T_{100}/L)^a$	40 (126)	0.3	91	80	0.3 - 1.1
100	20 (63)	0.3	92	80	0.3 - 1.5
Light troffer	60 (189)	2.5	86	80	<3.8
diffusers	40 (126)	1.0	92	90	<3.0
	20 (63)	1.0	95	90	<4.5
Perforated and	11-51 (35-160)	2.0	96	90	1.4-2.7
louvered ceiling diffusers	. ,			80	1.0-3.4

 $[^]a$ For SI units, $x_{0.25}$ /L and $T_{0.5}$ /L

Source: Reprinted by permission from ASHRAE Handbook, Fundamentals Volume, 1997.

Table 11-3 Performance Data for a Typical Linear Diffuser

Size,	Area,	Total Pressure,	Flow,			Throw,a ft	:
in.	ft ² /ft	in. wg	cfm/ft	NCb	Min.	Mid.	Max.
2	0.055	0.009	22	_	1	1	1
		0.020	33	_	4	4	4
		0.036	44	12	7	7	7
		0.057	55	18	9	9	10
		0.080	66	23	11	11	12
		0.109	77	27	13	14	16
		0.143	88	31	14	16	18
		0.182	99	34	15	17	20
		0.225	110	37	17	19	21
4	0.139	0.009	56	_	3	3	3
		0.020	83	_	9	9	9
		0.036	111	12	13	13	13
		0.057	139	18	16	16	17
		0.080	167	23	20	20	21
		0.109	195	27	22	23	24
		0.143	222	31	24	25	26
		0.182	250	34	27	27	27
		0.225	278	37	30	30	30
6	0.221	0.009	88	_	5	5	5
		0.020	133	_	10	10	10
		0.036	177	13	15	15	15
		0.057	221	19	18	18	18
		0.080	265	24	23	23	23
		0.109	310	28	25	25	25
		0.143	354	32	28	28	28
		0.182	398	35	31	31	31
		0.225	442	38	32	32	32

Multiplier Factor for Throw Value

Active Length,	at Terminal Velocity, ft/min					
ft	150	100	50			
1	0.5	0.6	0.7			
10 or continuous	1.6	1.4	1.2			

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Active Length,	NC Correction	Active Length,	NC Correction
	Confection		Conection
1	-10	10	0
2	-7	15	+2
4	-4	20	+3
6	-2	25	+4
8	-1	30	+5

^aMinimum throw values refer to a terminal velocity of 150 ft/min, middle to 100 ft/min, and maximum to 50 ft/min, for a 4 ft active section with a cooling temperature differential of 20 F. The multiplier factors listed at the bottom are applicable for other lengths. b Based on a room absorption of 80 dB referred to 10^{-12} W, and a 10 ft active section.

Table 11-4 Performance Data for a Typical Round Ceiling Diffuser

Size,	Neck Velocity,	Velocity Pressure,	Total Pressure,	Flow Rate,	Radiu	s of Diffus	sion,ª ft	
in.	ft/min	in. wg	in. wg	cfm	Min	Mid.	Max.	NC
6	400	0.010	0.026	80	2	2	4	_
	500	0.016	0.041	100	2	3	5	_
	600	0.023	0.059	120	2	4	6	14
	700	0.031	0.079	140	3	4	7	19
	800	0.040	0.102	160	3	5	8	23
	900	0.051	0.130	180	4	5	9	26
	1000	0.063	0.161	200	4	6	10	30
	1200	0.090	0.230	235	5	7	11	35
8	400	0.010	0.033	140	2	4	6	_
	500	0.016	0.052	175	3	4	7	15
	600	0.023	0.075	210	4	5	9	21
	700	0.031	0.101	245	4	6	10	26
	800	0.040	0.130	280	5	7	11	31
	900	0.051	0.166	315	5	8	13	34
	1000	0.063	0.205	350	6	9	14	37
	1200	0.090	0.292	420	7	11	17	44
10	400	0.010	0.027	220	3	4	7	_
	500	0.016	0.043	270	3	5	8	11
	600	0.023	0.062	330	4	6	10	17
	700	0.031	0.084	380	5	7	11	21
	800	0.040	0.108	435	5	8	13	26
	900	0.051	0.138	490	6	9	15	30
	1000	0.063	0.170	545	7	10	16	33
	1200	0.090	0.243	655	8	12	20	39
12	400	0.010	0.026	315	3	5	8	_
	500	0.016	0.042	390	4	6	10	11
	600	0.023	0.060	470	5	7	12	17
	700	0.031	0.081	550	6	8	13	22
	800	0.040	0.105	630	6	10	15	26
	900	0.051	0.134	705	7	11	17	30
	1000	0.063	0.166	785	8	12	19	33
	1200	0.090	0.236	940	10	14	23	39
18	400	0.010	0.030	710	5	7	12	_
	500	0.016	0.048	885	6	9	15	15
	600	0.023	0.069	1060	7	11	18	21
	700	0.031	0.093	1240	9	13	21	26
	800	0.040	0.120	1420	10	15	24	30
	900	0.051	0.153	1590	11	17	27	34
	1000	0.063	0.189	1770	12	19	30	37
	1200	0.090	0.270	2120	15	22	36	43

Table 11-4 Performance Data for a Typical Round Ceiling Diffuser (continued)

	Di	mensions	3		C diameter →
Size A	В	C	D	E	⊸ B diameter →
6	$6\frac{1}{2}$	11 ½	$1\frac{3}{4}$	11/8	Duct diameter Duct Ceiling
8	$8\frac{1}{2}$	$14\frac{3}{4}$	$2\frac{1}{8}$	$1\frac{1}{2}$	Size
10	$10\frac{1}{2}$	$18\frac{1}{4}$	$2\frac{7}{8}$	$2\frac{1}{8}$	3/4 D \ Open
12	$12\frac{1}{2}$	22	$3\frac{1}{8}$	$2\frac{3}{8}$	E v Closed
24	$24\frac{1}{2}$	$43\frac{1}{4}$	$7\frac{3}{4}$	$6\frac{5}{8}$	Gasket

^aMinimum radii of diffusion are to a terminal velocity of 150 ft/min, middle to 100 ft/min, and

maximum to 50 ft/min.

bThe NC values are based on a room absorption of 18 dB referred to 10⁻¹³ W (8 dB referred to

Table 11-5 Performance Data for an Adjustable-Type, High Sidewall Diffuser

		Flow,		Veloc.	Tb	tal Pressi	ше,					
Sizes.	A_{c}	Rate,	Veloc.,	Press.,		in. wg			Defl.,		Throw,	ft
in.	fil ²	cfm	ft/min	in. wg	0°	22½°	45°	NC	deg	Min.	Mid	Max.
8 × 4	0.18	70	400	0.010	0.017	0.019	0.029		0_	6	8	15
7×5									$22\frac{1}{2}$	5	6	12
6×6									45	3	4	8
10×4	0.22	90							0	7	10	17
8 × 5,									22]	6	8	14
7×6									45	3	5	9
12×4	0.26	105							0	7	11	19
10×5									22 	6	9	15
8 × 6									45	4	5	9
16×4	0.34	135							0	8	12	21
12×5									22]	6	10	17
10×6									45	4	б	11
18×4	0.39	155							0	9	13	23
14×5									$22\frac{1}{2}$	7	10	18
12×6									45	4	б	11
8×4	0.18	90	500	0.016	0.028	0.031	0.047		0	7	11	17
7×5									22 }	б	9	14
6×6									45	4	5	9
10×4	0.22	110							0	8	12	19
8×5									22 	6	10	15
7×6									45	4	б	10
12×4	0.26	130							0	9	13	21
10×5									22 	7	10	17
8 × 6									45	4	7	10
16×4	0.34	170						-	0	10	15	24
12×5									22 	8	12	19
10×6									45	5	8	11
18×4	0.39	195							0	11	16	25
14×5									$22\frac{1}{2}$	9	13	20
12×6									45	5	8	13

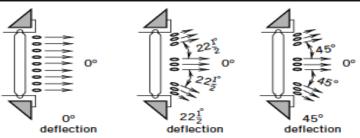
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Table 11-5 Performance Data for an Adjustable-Type, High Sidewall Diffuser (continued)

		Flow.		Veloc.	To	tal Pressi	ше,					
Sizes.	A_c ,	Rate,	Veloc.,	Press.,		in. wg			Defl.,		Throw,	ft
in.	fl ²	cfm	ft/min	in. wg	0°	22½°	45°	NC	deg	Min.	Mid.	Max.
8×4,	0.18	110	600	0.022	0.038	0.043	0.064	10	0	9	13	19
7×5,									$22\frac{1}{2}$	7	10	15
6×6									45	4	7	10
10×4,	0.22	130						10	0	9	15	21
8×5,									$22\frac{1}{2}$	7	12	17
7×6									45	5	7	10
12×4,	0.26	155						11	0	10	16	23
10×5,									$22\frac{1}{2}$	8	13	18
8×6									45	5	8	11
16×4,	0.34	205						12	ο,	12	19	26
12×5,									$22\frac{1}{2}$	10	15	21
10×6									45	6	9	13
18×4,	0.39	235						13	ο,	13	19	28
14×5,									$22\frac{1}{2}$	10	15	22
12×6									45	7	10	14
8×4,	0.18	125	700	0.030	0.052	0.058	0.088	15	ο,	10	15	20
7×5,									$22\frac{1}{2}$	8	12	16
6×6									45	5	7	10
10×4	0.22	155						15	0,	11	16	23
8×5,									$22\frac{1}{2}$	9	13	18
7×6									45	6	8	11
12×4	0.26	180						16	0,	12	17	24
10 × 5,									$22\frac{1}{2}$	10	14	19
8×6									45	6	9	12
16×4,	0.34	240						17	0,	14	20	28
12 × 5,									$22\frac{1}{2}$	11	16	22
10×6									45	7	10	14
18×4,	0.39	275						18	0	15	22	30
14×5,									$22\frac{1}{2}$	12	18	24
12×6,									45	8	11	15
8 × 4,	0.18	145	800	0.040	0.069	0.078	0.117	19	0	11	16	22
7×5,									$22\frac{1}{2}$	9	13	18
6×6		100							45	6	8	11
10×4,	0.22	175						19	0	13	17	24
8 × 5,									$22\frac{1}{2}$	10	14	19
7×6	0.25	210						20	45	6	9	12
12×4,	0.26	210						20	0	14	19	26
10 × 5,									$22\frac{1}{2}$	11	15	21
8×6	0.74	220							45	7	9	13
16×4	0 34	270						21	0	16	22	30

Table 11-5 Performance Data for an Adjustable-Type, High Sidewall Diffuser (continued)

		Flow.		Veloc.	To	otal Pressu	re,					
Sizes,	A_{ς}	Rate,	Veloc.,	Press.,		in. wg			Defl.,		Throw,	ft
in.	πΣ	cfm	ft/min	in. wg	0°	22 ½°	45°	NC	deg	Min.	Mid.	Max.
10×4,	0.22	220						25	0	16	19	27
8×5									$22\frac{1}{2}$	13	15	22
7×6									45	8	10	13
12×4	0.26	260						26	0	17	21	19
10×5									$22\frac{1}{2}$	14	17	23
8×6									45	8	11	15
16×4	0.34	340						27	0	20	24	33
12×5									$22\frac{1}{3}$	16	19	26
10×6									45	10	12	17
18×4	0.39	390						28	0	21	26	36
14×5									$22\frac{1}{3}$	17	21	29
12×6									45	11	13	18



<u>Example 2</u>: Suppose the room of Figure 1 is located in the southern latitudes where overhead systems are recommended. Select a round ceiling diffuser system and a high sidewall system. Also select a return grille.

Given: 250 cfm air quantity Required:

Select a round ceiling diffuser, select high sidewall grille, and select a return grille.

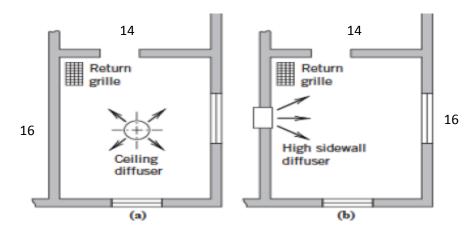


Figure 1

Solution: The data of Table 11.1 with information from Table 11.2 and 11.4 will be used to select a **ceiling diffuser**. The characteristic length is 7 or 8 ft and the throw-to-length ratio is 0.8; then

$$x_{50}/L = 0.8$$
 \rightarrow $x_{50}=0.8 \times (7) = 5.6 \text{ ft}$

Using correction factor: $x_{50}=5.6/0.75=7.5$

The best choice would be

Size, in	Throw, ft	NC	ΔP_0 , in. wg
10	7 ½	10	0.035

The throw is larger than desired, but the throw-to-length ratio is within the range to give a minimum *ADPI* of 76 percent. **Figure 1a** shows this application.

A high sidewall diffuser may be selected from Table 11.2. In this case the throw-to-length ratio should be about 1.8 and the characteristic length is 14 ft; then

$$x_{50} / L = 1.8 \rightarrow x_{50} = 1.8 \times (14) = 25.2 \text{ ft}$$

At 240 cfm, pressure drop at 22 ½ degree spread would be 0.058:

At 250 cfm, pressure drop at 22 ½ degree spread would be acceptable

$$\Delta P = (\frac{250}{240})^2 \times 0.058 = 0.063 \text{ in. wg}$$

The best choice would be

Size, in	Throw, ft	NC	ΔP_0 , in. wg
16 x4			
12 x 5	25	18	0.063
10 x 6			

RETURN GRILLES

Velocities thru return grilles depend on (1) the static pressure loss allowed and (2) the effect on occupants or materials in the room. In determining the pressure loss, computations should be based on the free velocity thru the grille, not on the face velocity, since the orifice coefficient may approach 0.7. In general the following velocities may be used (see table 1-7):

Table 1-7 Recommended return velocities for different applications.

GRILLE LOCATION	FPM OVER GROSS AREA
Commercial	
Above occupied zone	800 and above
Within occupied zone not near seats	600-800
Within occupied zone near seats	400-600
Door or wall louvers	500-1000
Undercutting of doors	600*
Industrial	800 and above
Residential	400

^{*}Thru undercut area

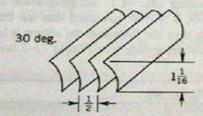
		Core Velocity,		en res					
		fpm	200	300	400	500	600	700	800
		Velocity Pressure.						MET LIN	
		in. wg	0.002	0.006	0.010	0.016	0.023	0.031	0.040
A. ft ²	Sizes, in.	Static Pressure,	-0.011	-0.033	-0.055	-0.088	0.126		
0.34		in. wg	70	100	135	170	-0.126	-0.170	-0.22
0.0	10×6	NC ^a	,0	100	13	20	205 25	240	270
0.39		cfm	80	115	155	195	235	30	33
	12×6	NC	- 00	113	14	21	26	275	310
0.46		cfm	90	140	185	230	275	31	34
	14×6	NC	,,,	140	15	22	27	320	370
	10×8						21	32	35
0.52	24×4	cfm	105	155	210	260	310	200	
	16×6	NC	100	133	16	23		365	415
0.60	28×4	cfm	120	180	240	300	28	33	36
	18×6	NC	* 2017	100	17		360	420	480
	12×8				1,	24	29	34	37
0.69	30×4	cfm	140	205	275	245		H.H.	
	20×6	NC	140	205	17	345	415	485	550
	14×8				1,	24	29	34	37
	12×10								
0.81	36×4	cfm	160	245	205		AND THE REAL PROPERTY.		
	22×6	NC	100	245	325	405	485	565	650
	16×8			10	18	25	30	35	38
	14×10								
0.90	40×4	cfm	180	270		The state of the s			
	26×6	NC	100	270	360	450	540	630	720
	18×8			11	19	26	31	36	39
	16×10								
	12×12								
.07	48×4	cfm	216						
	30×6	NC	215	320	430	535	640	750	855
	18×10	110		12	20	27	32	37	40
	14×12								10
.18	34×6	-	222						
might.	24×8	cfm	235	355	470	590	710	825	945
	20×10	NC		13	21	28	33	38	41
	16×12					中华 八十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二十二	- 410 10 2004	30	41
34	60×4	Allega Branch							
	36×6	cfm	270	400	535	670	805	940	1070
	18×12	NC		13	21	28	33		
	16 × 14				VIEW (AND	PERMIT	33	38	41
60		-							
	30×8	cfm	320	480	640	800	060		1000
	24×10	NC		14	22		960	1120	1280
	22×12			-	-	29	34	39	42
Althor.	18×14								

continues

Table 11 .0	'erformance	Data for	One	Type of	D		
			-	Type of	Keturn	Unille	(continued)

		Core Velocity, fpm	200	300	400	continued)			
		Velocity Pressure, in. wg	0.002	0.006	0.010	0.016	600	700	800
A. ft²	Sizes, in.	Static Pressure, in, wg	-0.011	-0.033	-0.055	-0.088	-0.126	0.031	0.040
1.80	48 × 6 36 × 12 30 × 10	efm NC	360	540 15	720 23	900	1080 35	-0.170 1260 40	-0.220 1440 43
2.08	24×12 60×6 40×8 36×10 30×12	cfm NC	415	625 16	830 24	1040 31	1250 36	1460 41	1660 44
2.45	24×14 20×16 48×8 26×14	cfm NC	490	735 17	980	1220	1470	1720	1960
2.78	24 × 16 36 × 12 30 × 14 26 × 16	cfm NC	555	835 18	25 1110 26	32 1390 33	37 1670 38	42 1950 43	45 2220 46
3.11	24×18 40×12 36×14	cfm NC	620	935 19	1240 27	1560 34	1870 39	2180	2490 47
3.61	30 × 16 24 × 20 48 × 12 36 × 16 24 × 24	cfm NC	720	1080 20	1440 28	1800 35	2170 40	2530 45	2890 48

*Based on a room absorption of 8 dB, with respect to 10-12 watts, and one return.



Example: Small store dimensions: $32 \times \frac{23}{} \times 16$ ft

Ceiling - flat

Load – equally distributed Air quantity – 2000 cfm Temp difference – 25 F

Find: Number of outlets, Size of outlets,

Solution:

-The minimum blow is 75% of the room width for the given condition of equally distributed heat load. Therefore, the minimum blow necessary is: $23 \times 0.75 = 17.3$ ft

- The maximum blow is the width of the room =32 ft
- The blow of 17.5 to 34 ft.

- No. of outlets=
$$\frac{2000}{500} = 4$$

- nominal size 24 in. x 6 in

$$k = \frac{2000}{32 \times 16} = 3.9$$

TABLE 1-8 - WALL OUTLET RATINGS, FOR COOLING ONLY

For Flat Ceilings

STATIC P		Su s		2214		0.1	375 FPM Ser B = .013, 221/4" = .015					500 FFM 5ir 8 = .024, 221/5" = .028				Sau B		22 M		041	
STANDAR	OUTLET	Ser 8 = .01, 22½° = .01 45° = .01				45" = .019					45" = .035				Sir 8 = .051, 221/5" = .061 45" = .08						
STATIC PRESSURE WITH METERING PLATE		Ser 8 = .01, 221/4" = .015 45" = .028			Ser 8 = .024, 22½° = .043 45° = .065				Str 8 = .061, 221/6" = .082 45" = .118				Ser B = .175, 221/5° = .19 45° = .27								
Nom. Size of Outlet	Vene	Air Quan-	Mew		20	(P) 25	Air Quan-	Blow	Tem;	90 DIM	(F)	Air Quan-	New	Tem 15	90 Diff	(F) 25	Air Oven-	Blow	Tem 15	p. Diff.	(F)
(and Free Area)	Setting	(clm)	(91)	15 Mir	. Og	_	(clm)	(91)		a Cig		(cfm)	(11)		. Clg		(clm)	(M)		n Cig	
# × 4 (16.9)	Straight 221/4° 45°	30	3.5 2.5 1.8	6.5 6.0	7.0 6.5 6.0	7,0 6.5 6.5	44	7.0 5.1 3.5	7.5 6.5 6.5	7.5 7.0 6.5	8.0 7.0 7.0	59	10.0 7.5 5.0	7.5 7.0 6.5	8.0 7.5 6.5	8.5 7.5 7.0	19	17.0 13.0 9.0	8.5 7.5 6.5	9.0 7.5 7.0	9.0 8.0 7.0
10 x 4 (21.7)	Straight 22 1/5 * 45*	37	3.5 2.5 1.8	6.5 6.5 6.0	7.0 6.5 6.0	7.5 7.0 6.5	57	7.4 5.5 3.7	7.5 6.5 6.5	7.5 7.0 6.5	8.0 7.0 7.0	75	10.5 8.0 5.4	7.5 7.0 6.5	8.0 7.5 6.5	8.5 7.5 7.0	112	18.0 13.0 9.0	8.5 7.5 6.5	9,0 8,0 7,0	9.0 8.0 7.0
12 × 4 (24.6)	Straight 2216* 45*	44	3.5 2.5 1.8	33 33 39	7.0 6.5 6.5	7.5 7.0 4.5	44	7.5 5.5 3.9	7.5 7.0 6.5	7.5 7.0 6.5	8.0 7.5 7.0	91	11.0 8.1 5.5	8.0 7.0 6.5	8.0 7.5 7.0	8.5 7.5 7.0	136	18.0 13.0 9.0	8.5 7.5 6.5	9,0 8.0 7.0	9.5 8.5 7.0
16 x 4 (35.9)	Strolght 221/5° 45°	61	3.7 2.7 2.0	7.0 6.5 6.0	7.0 6.5 6.5	7.5 7.0 6.5	92	7.9 6.0 4.0	7.5 7.0 6.5	7.5 7.0 4.5	8.0 7.5 7.0	122	11,0 8,1 5,5	8.0 7.0 6.5	8,0 7,5 7,0	8.5 7.5 7.0	183	19,0 14,0 10,0	8.5 7.5 6.5	9.0 8.0 7.0	9.5 8.5 7.5
20 m 4 (45.5)	Stroloht 22 % 45*	77	4.0 3.0 2.0	7.0 6.5 6.0	7.0 6.5 6.5	7.5 7.0 6.5	115	8.0 6.0 4.0	7.5 7.0 6.5	8.0 7.0 6.5	8.0 7.5 7.0	154	11.5 8.5 6.0	8.0 7.5 6.5	8.0 7.5 7.0	8.5 8.0 7.0	231	20.0 15.0 10.0	8.5 7.5 4.5	9.0 8.0 7.0	9.5 8.5 7.5
24 × 4 (55.0)	Straight 22 ¼° 45°	93	4.1 3.1 2.0	7.0 6.5 6.0	7.0 7.0 6.5	7.5 7.0 6.5	139	8.0 6.0 4.0	7.5 7.0 6.5	8.0 7.0 6.5	8.0 7.5 7.0	185	11.5 8.5 6.0	8.0 7.5 6.5	8.0 7.5 7.0	8.5 8.0 7.0	278	20.0 15.0 10.6	8.5 7.5 4.5	9.0 8.0 7.0	10.0 8.5 7.5
30 x 4 (68.3)	Strolight 221/5° 45°	114	4.2 3.1 2.1	7.0 4.5 6.0	7.0 7.0 6.5	7.5 7.0 4.5	175	8.0 6.0 4.0	7.5 7.0 6.5	8.0 7.3 6.5	8.0 7.5 7.0	233	12.0 9.0 6.0	8.0 7.5 6.5	8.0 7.5 7.0	8.5 8.0 7.0	349	21.0 16.0 11.0	8.5 7.5 7.0	9.5 8.0 7.0	10.0 8.5 7.5
36 x 4 (83.5)	Strolght 22 ½° 45°	140	4.4 3.3 2.2	7.0 6.5 6.0	7.5 7.0 6.5	7.5 7.0 6.5	210	8.0 6.0 4.0	7.5 7.0 6.5	8.0 7.5 6.5	8.0 7.5 7.0	279	12.0 9.0 6.0	8.0 7.5 6.5	8.5 7.5 7.0	9,0 8,0 7,0	420	21,0 16,0 11,0	9.0 7.5 7.0	9.5 8.5 7.0	10.0 8.5 7.5
8 x 6 (24.5)	Straight 22 ½ * 45*	52	5.0 3.8 2.5	7.5 7.0 6.0	7.5 7.0 6.5	8.0 7.5 6.5	77	9.5 7.0 4.8	8.0 7.0 6.5	8.0 7.5 7.0	8.5 8.0 7.0	103	13.0 10.0 6.0	8.5 7.5 7.0	9.0 8.0 7.0	9.0 8.5 7.5	155	24.0 18.0 12.0	8.5 8.0 7.0	10.0 8.5 7.5	10.5 9.5 8.0
10 × 6 (34.0)	Strolight 221/5° 45°	64	5.5 4.1 2.8	7.5 7.0 4.5	8.0 7.5 7.0	8.0 7.5 7.0	98	10,0 7.5 5.0	8.0 7.5 7.0	8.5 8.0 7.0	9.0 8.5 7.5	131	15.0 11.0 7.0	9.0 8.0 7.0	9.5 8.5 7.5	10.0 9.0 7.5	196	27.0 20.0 14.0	10.0 8.5 7.5	10.5 9.0 7.5	11.5 10.0 8.0
12 x 6 (41.6)	Strolght 221/4" 45"	80	6.0 4.5 3.0	7.5 7.0 6.5	8.0 7.5 7.0	8.5 7.5 7.0	119	11.0 8.1 5.5	8.0 7.5 7.0	9.0 8.0 7.0	9.5 8.5 7.5	159	15.0 11.0 7.0	9.0 8.0 7.0	9.5 8.5 7.5	10.0 9.0 7.5	234	28.0 21.0 14.0	10.0 9.0 7.5	11.0 9.5 8.0	11.5 10.0 8.0
16 × 6 (56.6)	Strolght 22 1/5 * 45*	107	6.2 4.7 3.2	8.0 7.0 6.5	8.0 7.5 7.0	8.5 7.5 7.0	161	12.0 9.0 4.0	8.5 8.0 7.0	9.0 8.0 7.0	9.5 8.5 7.5	214	14.0 12.0 8.0	9.5 8.5 7.5	10.0 9.0 7.5	9.5 8.0	321	30,0 22,0 15,0	11.0 9.5 7.5	11.5 10.0 8.0	12.5 10.5 8.5
20 x 6 (71.5)	Strolight 22 1/3" 45"	135	5.6 5.0 3.2	8.0 7.5 7.0	8.5 7.5 7.0	9.0 8.0 7.5	202	12.0 7.0 6.6	9.0 8.0 7.0	9.5 8.5 7.5	10.0 9.0 7.5	269	17.0 13.0 9.0	9.5 8.5 7.5	9.0 9.0 8.0	9.5 8.0	403	32.0 24.0 16.0		12.0 10.0 8.5	13,0 11,0 9.0
24 x 6 (86.5)	Strolght 2215° 45°	162	7.0 5.1 3.5	8.0 7.5 7.0	8.5 8.0 7.0	9.0 8.0 7.5	243	13,0 10,0 4,5	9,0 8.0 7.0	9.5 8.5 7.5	10.0 9.0 8.0	324	18.0 13.0 9.0	10.0 8.5 7.5	10.5 9.0 8.0	11.0 10.0 8.5	486	33.0 25.0 17.0	12.0 10.0 8.0	12.5 10.5 8.5	
30 x 6 (109.0)	Straight 22 1/5 ° 45°	203	7.0 5.4 3.5	8.5 7.5 7.0	8.5 8.0 7.0	9.5 8.0 7.5	304	13.0 10.0 4.5	9.0 8.0 7.5	10.0 9.0 7.5	10.5 9.0 8.0	406	19.0 14.0 10.0	10.0 9.0 7.5	11.0 9.5 8.0	11.5 10.0 8.5	401	34.0 25.0 17.0	10.0 8.0	12.5 10.5 9.0	13.5 11.5 9.0
36 x 6 (131.3)	Strolght 221/5° 45°	245	7.1 5.5 3.5	8.5 7.5 7.0	9,0 8,0 7,5	9.5 8.5 7.5	368	13.0 10.0 6.5	9.5 8.5 7.5	10.0 9.0 8.0	10.5 9.5 8.0	490	19.0 14.0 10.0	10.0 9.0 8.0	11.0 9.5 8.0	12.0 10.0 8.5	735	35.0 26.0 18.0	12.0 10.0 8.5	13.0 10.5 9.0	14,0 11.5 9.5
	le -	_						K	FAC	TOR											
Max Cle Owlet W	ell Area		:	9.0				1	9.0				1	4.0					9.4		
Min Cfm, Outlet W	/Sq ft /oil Area			6.7					5.7					4.2					2.9		