

Lecture 10 - Flexure

Lecture Goals

- Doubly Reinforced beams

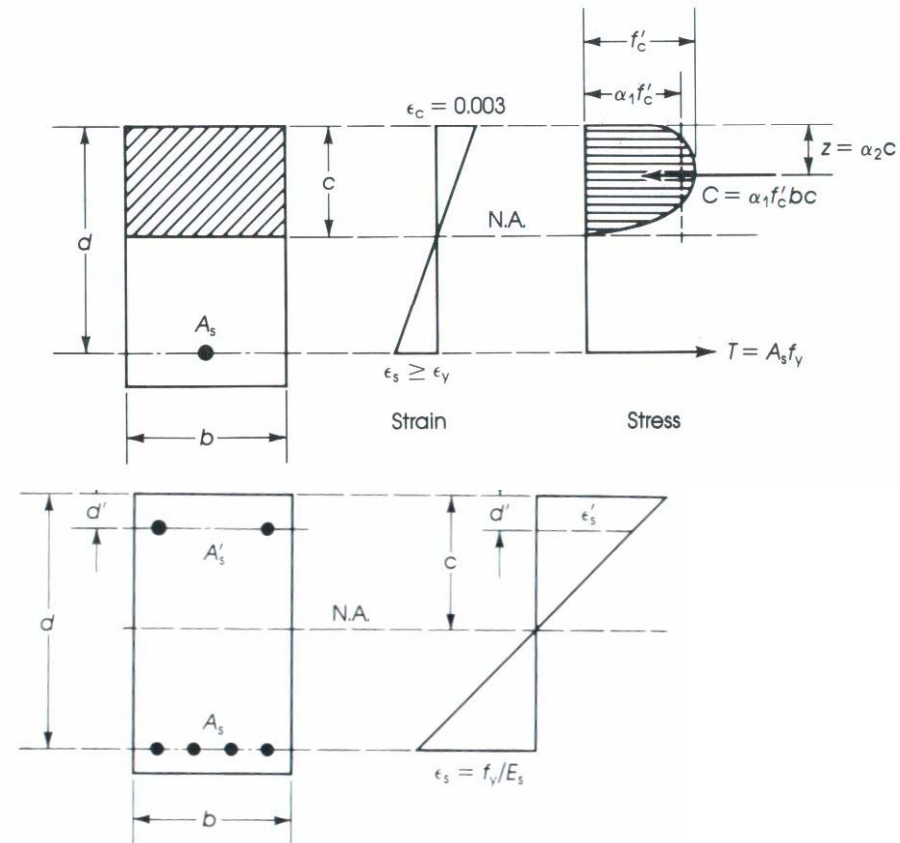
Analysis of Doubly Reinforced Sections

Effect of Compression Reinforcement on the Strength and Behavior

Less concrete is needed to resist the T and thereby moving the neutral axis (NA) up.

$$T = A_s f_y$$

$$C = T$$



Analysis of Doubly Reinforced Sections

Effect of Compression Reinforcement on the Strength and Behavior

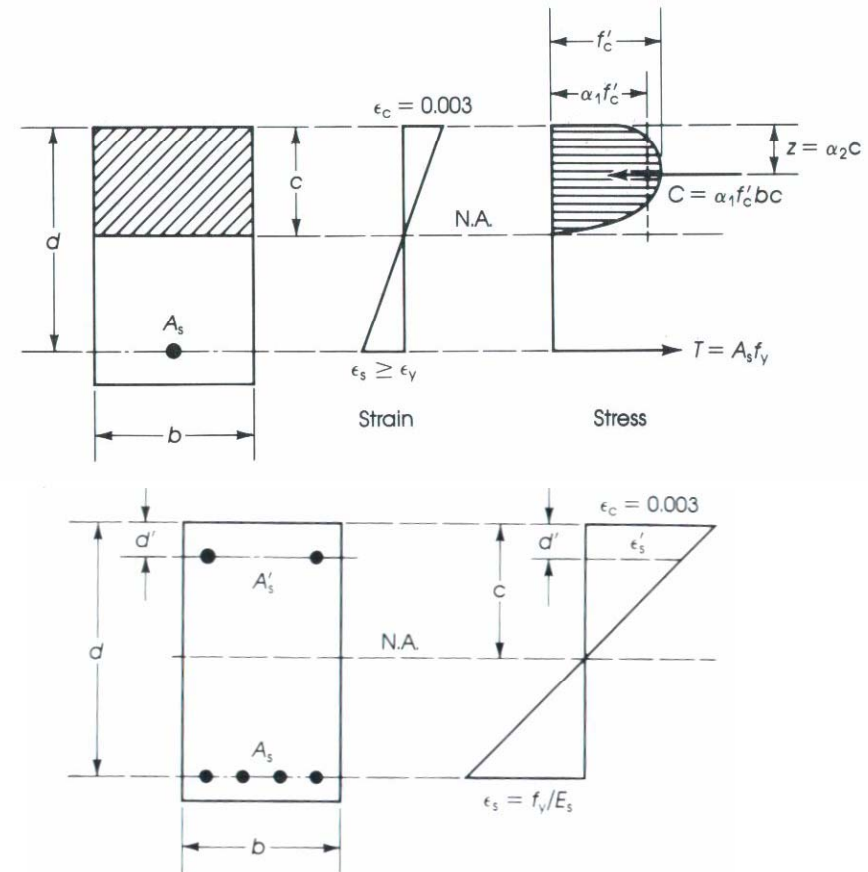
Singly Reinforced $\Rightarrow$

$$C = C_c ; M_n = A_s f_y \left(d - \frac{a_1}{2} \right)$$

Doubly Reinforced $\Rightarrow$

$$C = C_c + C'_s ; M_n = A_s f_y \left(d - \frac{a_2}{2} \right)$$

and $(a_2 < a_1)$



Reasons for Providing Compression Reinforcement

- Reduced sustained load deflections.
 - Creep of concrete in compression zone
 - transfer load to compression steel
 - reduced stress in concrete
 - less creep
 - less sustained load deflection

Reasons for Providing Compression Reinforcement

Effective of compression reinforcement on sustained load deflections.

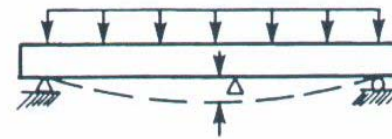
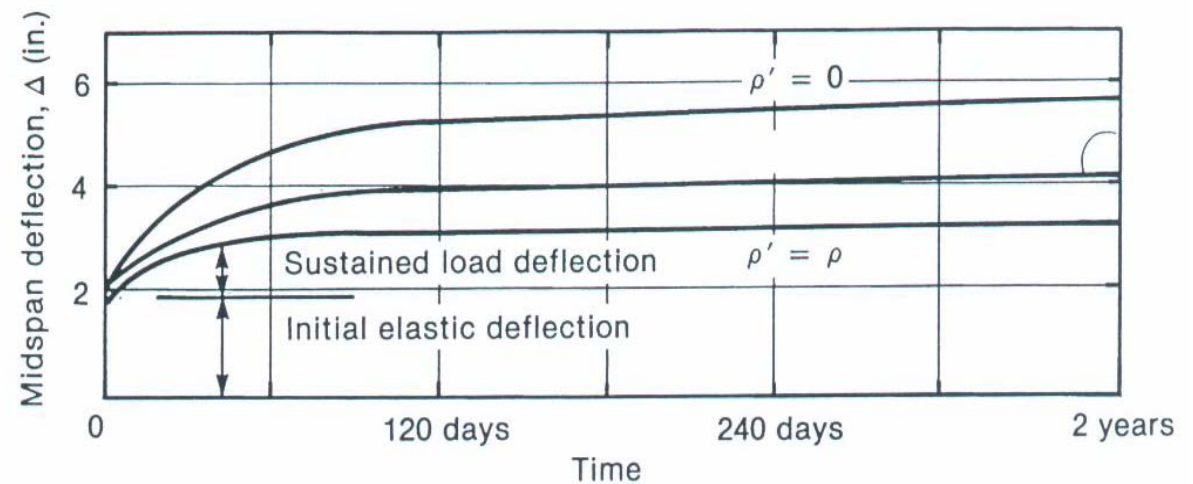


Fig 5-14 MacGregor



Reasons for Providing Compression Reinforcement

- Increased Ductility
reduced stress block depth $\longrightarrow$ increase
in steel strain larger curvature are obtained.

Reasons for Providing Compression Reinforcement

Effect of compression reinforcement on strength and ductility of under reinforced beams.

$$\rho < \rho_b$$

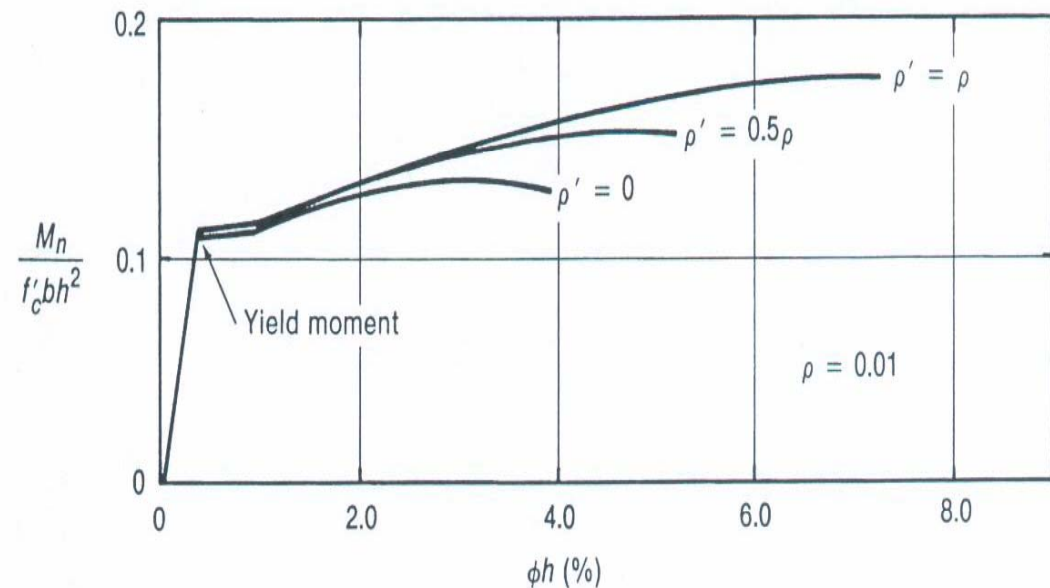


Fig 5-15 MacGregor

Reasons for Providing Compression Reinforcement

- Change failure mode from compression to tension. When $\rho > \rho_{bal}$, addition of A_s strengthens.

Compression zone $\longrightarrow$ allows tension steel to yield before crushing of concrete.

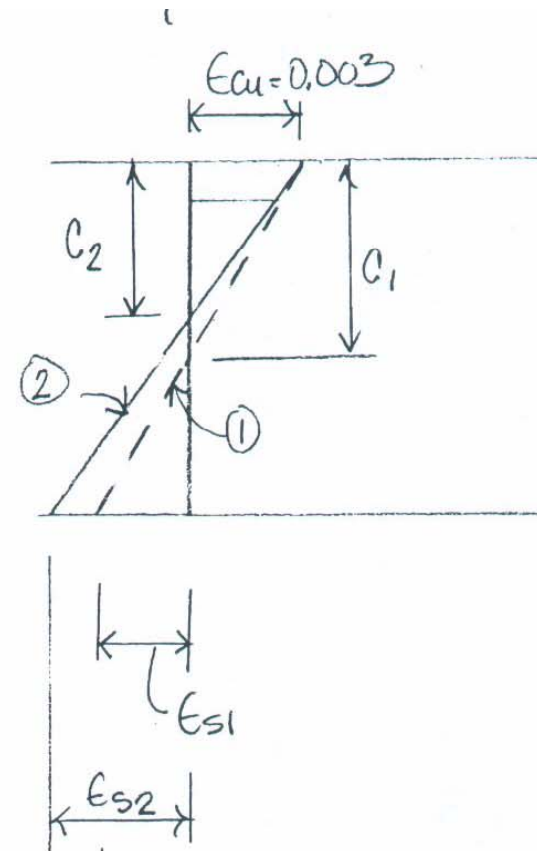
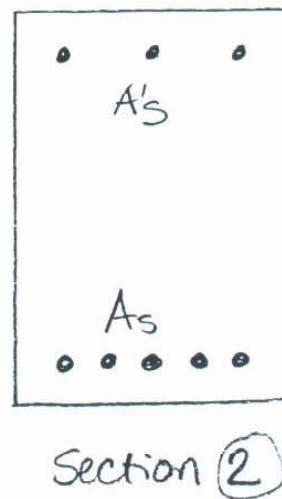
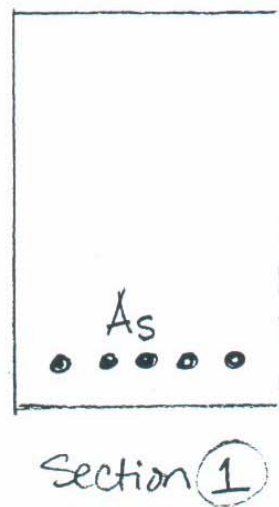
Effective reinforcement ratio = $(\rho - \rho')$

Reasons for Providing Compression Reinforcement

- Eases in Fabrication
use corner bars to hold & anchor stirrups.

Effect of Compression Reinforcement

Compare the strain distribution in two beams with the same A_s



Effect of Compression Reinforcement

Section 1:

$$T = A_s f_s$$

$$T = C_{c1} = 0.85 f'_c b a = 0.85 f'_c b \beta_1 c_1$$

$$c_1 = \frac{A_s f_s}{0.85 f'_c b \beta_1}$$

Section 2:

$$T = A_s f_s$$

$$T = C'_s + C_{c1}$$

$$= A'_s f'_s + 0.85 f'_c b a_2$$

$$= A'_s f'_s + 0.85 f'_c b \beta_1 c_2$$

$$c_2 = \frac{A_s f_s - A'_s f'_s}{0.85 f'_c b \beta_1}$$

Addition of A'_s strengthens compression zone so that less concrete is needed to resist a given value of T . $\longrightarrow$ NA goes up ($c_2 < c_1$) and ϵ_s increases ($\epsilon_{s2} > \epsilon_{s1}$).

Doubly Reinforced Beams

Four Possible Modes of Failure

- Under reinforced Failure
 - (Case 1) Compression and tension steel yields
 - (Case 2) Only tension steel yields
- Over reinforced Failure
 - (Case 3) Only compression steel yields
 - (Case 4) No yielding Concrete crushes

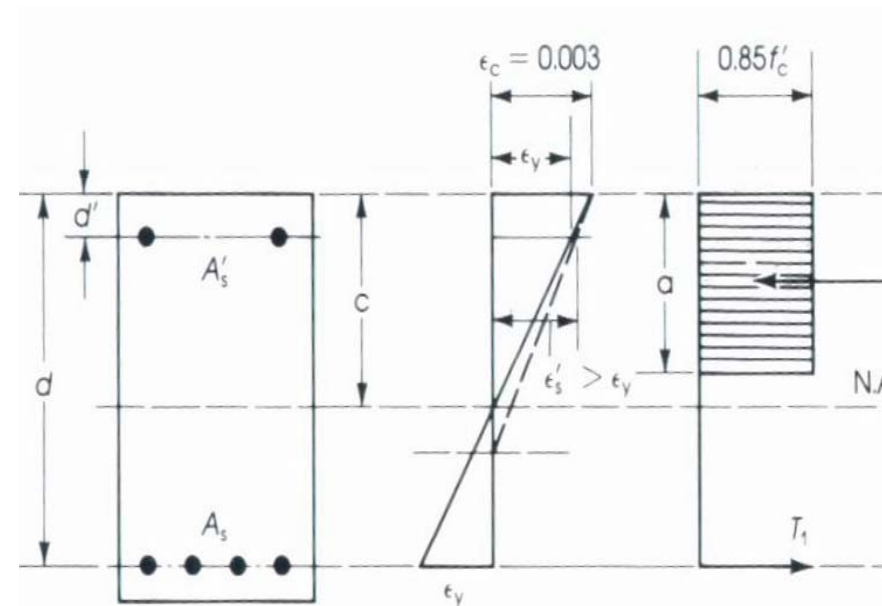
Analysis of Doubly Reinforced Rectangular Sections

Strain Compatibility Check

Assume ϵ_s' using similar triangles

$$\frac{\epsilon_s}{(c - d')} = \frac{0.003}{c} \Rightarrow$$

$$\epsilon_s = \frac{(c - d') * 0.003}{c}$$



Analysis of Doubly Reinforced Rectangular Sections

Strain Compatibility

Using equilibrium and find a

$$T = C'_c + C'_s \Rightarrow a = \frac{(A_s - A'_s) f_y}{0.85 f'_c b}$$

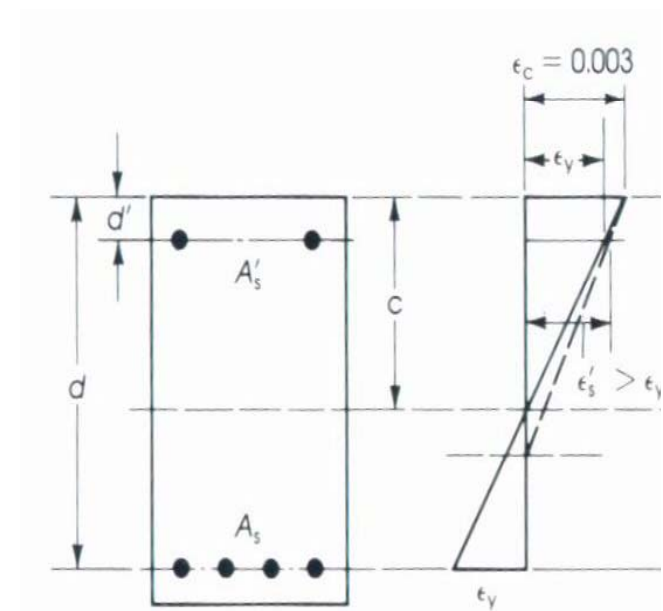
$$c = \frac{a}{\beta_1} = \frac{(A_s - A'_s) f_y}{\beta_1 (0.85 f'_c b)} = \frac{(\rho - \rho') d f_y}{\beta_1 (0.85 f'_c)}$$

Analysis of Doubly Reinforced Rectangular Sections

Strain Compatibility

The strain in the compression steel is

$$\begin{aligned}\epsilon'_s &= \left(1 - \frac{d'}{c}\right) \epsilon_{cu} \\ &= \left(1 - \frac{\beta_1 (0.85 f'_c) d'}{(\rho - \rho') d f_y}\right) 0.003\end{aligned}$$

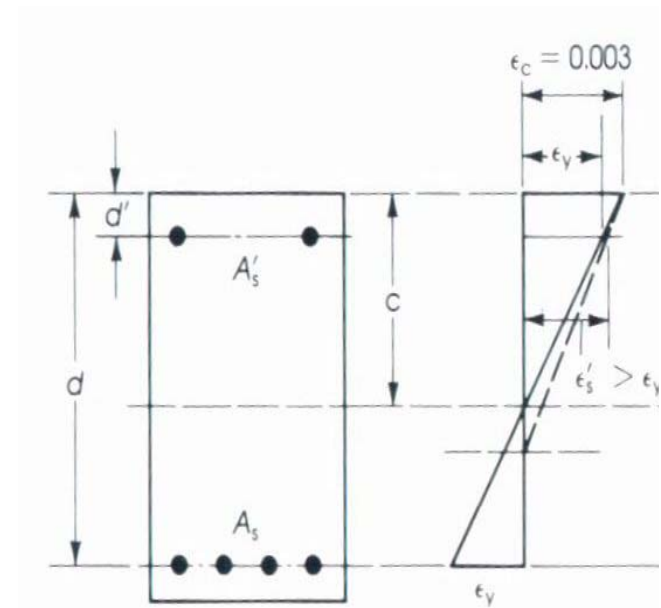


Analysis of Doubly Reinforced Rectangular Sections

Strain Compatibility
Confirm

$$\epsilon'_s \geq \epsilon_y = \frac{f_y}{E_s}; \quad \epsilon_s \geq \epsilon_y$$

$$\epsilon'_s = \left(1 - \frac{\beta_1 (0.85 f'_c) d'}{(\rho - \rho') d f_y} \right) 0.003 \geq \frac{f_y}{E_s} = \frac{f_y}{29 \times 10^6}$$



Analysis of Doubly Reinforced Rectangular Sections

Strain Compatibility

Confirm

$$-\frac{\beta_1 (0.85 f'_c) d'}{(\rho - \rho') d f_y} \geq \frac{f_y - 87000}{87000}$$

$$(\rho - \rho') \geq \left(\frac{\beta_1 (0.85 f'_c) d'}{d f_y} \right) \left(\frac{87000}{87000 - f_y} \right)$$

Analysis of Doubly Reinforced Rectangular Sections

If the statement is true than

$$M_n = (A_s - A'_s) f_y \left(d - \frac{a}{2} \right) + A'_s f_y (d - d')$$

else the strain in the compression steel

$$f_s = E \varepsilon_s$$

Analysis of Doubly Reinforced Rectangular Sections

Strain

Compute the stress in the compression steel.

$$f'_s = 29 \times 10^6 \left(1 - \frac{\beta_1 (0.85 f'_c) d'}{(\rho - \rho') d f_y} \right) 0.003$$

Analysis of Doubly Reinforced Rectangular Sections

Go back and calculate the equilibrium with f_s'

$$T = C'_c + C'_s \Rightarrow a = \frac{(A_s f_y - A'_s f_s')}{0.85 f'_c b}$$

$$c = \frac{a}{\beta_1}$$

Iterate until the c value is adjusted for the f_s'

$$f'_s = \left(1 - \frac{d'}{c}\right) 87000$$

Analysis of Doubly Reinforced Rectangular Sections

Go back and calculate the moment capacity of the beam

$$M_n = (A_s f_y - A'_s f'_s) \left(d - \frac{a}{2} \right) + A'_s f'_s (d - d')$$

Limitations on Reinforcement Ratio for Doubly Reinforced beams

Lower limit on ρ (ACI 10.5)
same as for single reinforce beams.

$$\rho_{\min} = \frac{3\sqrt{f'_c}}{f_y} \geq \frac{200}{f_y}$$

Example: Doubly Reinforced Section

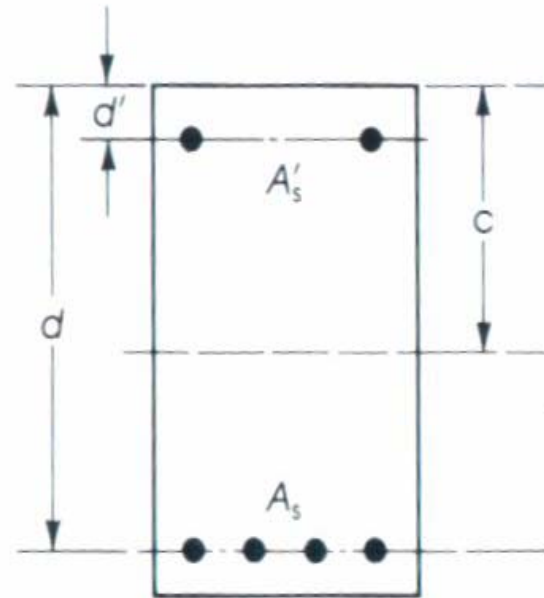
Given:

$$f'_c = 4000 \text{ psi} \quad f_y = 60 \text{ ksi}$$

$$A'_s = 2 \text{ #5} \quad A_s = 4 \text{ #7}$$

$$d' = 2.5 \text{ in.} \quad d = 15.5 \text{ in.}$$

$$h = 18 \text{ in.} \quad b = 12 \text{ in.}$$



Calculate M_n for the section for the given compression steel.

Example: Doubly Reinforced Section

Compute the reinforcement coefficients, the area of the bars #7 (0.6 in²) and #5 (0.31 in²)

$$A_s = 4(0.6 \text{ in}^2) = 2.4 \text{ in}^2$$

$$A'_s = 2(0.31 \text{ in}^2) = 0.62 \text{ in}^2$$

$$\rho = \frac{A_s}{bd} = \frac{2.4 \text{ in}^2}{(12 \text{ in.})(15.5 \text{ in.})} = 0.0129$$

$$\rho' = \frac{A'_s}{bd} = \frac{0.62 \text{ in}^2}{(12 \text{ in.})(15.5 \text{ in.})} = 0.0033$$

Example: Doubly Reinforced Section

Compute the effective reinforcement ratio and minimum ρ

$$\rho_{eff} = \rho - \rho' = 0.0129 - 0.0033 = 0.00957$$

$$\rho = \frac{200}{f_y} = \frac{200}{60000} = 0.00333 \text{ or } \frac{3\sqrt{f_c}}{f_y} = \frac{3\sqrt{4000}}{60000} = 0.00316$$

$$\rho \geq \rho_{min} \Rightarrow 0.0129 \geq 0.00333 \text{ OK!}$$

Example: Doubly Reinforced Section

Compute the effective reinforcement ratio and minimum ρ

$$\begin{aligned}(\rho - \rho') &\geq \left(\frac{\beta_1 (0.85 f'_c) d'}{d f_y} \right) \left(\frac{87000}{87000 - f_y} \right) \\ &\geq \left(\frac{0.85 (0.85 (4 \text{ ksi})) (2.5 \text{ in.})}{60 \text{ ksi} (15.5 \text{ in.})} \right) \left(\frac{87}{87 - 60} \right) = 0.0398\end{aligned}$$

$0.00957 \not\geq 0.0398$ Compression steel has not yielded.

Example: Doubly Reinforced Section

Compute the effective reinforcement ratio and minimum ρ

$$\begin{aligned} f'_s &= 29 \times 10^6 \left(1 - \frac{\beta_1 (0.85 f'_c) d'}{(\rho - \rho') d f_y} \right) 0.003 \\ &= 87 \left(1 - \frac{0.85 (0.85 (4 \text{ ksi})) (2.5 \text{ in.})}{(0.00957) (15.5 \text{ in.}) (60 \text{ ksi})} \right) = 16.37 \text{ ksi} \end{aligned}$$

Use an iterative technique to find f'_s

Example: Doubly Reinforced Section

Compute the iterative values (1)

$$c = \frac{A_s f_y - A'_s f'_s}{0.85 f_c \beta_1 b} = \frac{(2.4 \text{ in}^2)(60 \text{ ksi}) - (0.62 \text{ in}^2)(16.37 \text{ ksi})}{0.85(4 \text{ ksi})(0.85)(12 \text{ in.})}$$

$$c = 3.86 \text{ in.}$$

$$\begin{aligned} f'_s &= E_s \varepsilon'_s = 29 \times 10^6 \left(1 - \frac{d'}{c} \right) 0.003 = 87 \left(1 - \frac{(2.5 \text{ in.})}{(3.86 \text{ in.})} \right) \\ &= 30.65 \text{ ksi} \end{aligned}$$

Use an iterative technique to find f'_s

Example: Doubly Reinforced Section

Compute the iterative values (2)

$$c = \frac{A_s f_y - A'_s f'_s}{0.85 f_c \beta_1 b} = \frac{(2.4 \text{ in}^2)(60 \text{ ksi}) - (0.62 \text{ in}^2)(30.65 \text{ ksi})}{0.85(4 \text{ ksi})(0.85)(12 \text{ in.})}$$

$$c = 3.604 \text{ in.}$$

$$\begin{aligned} f'_s &= E_s \varepsilon'_s = 29 \times 10^6 \left(1 - \frac{d'}{c} \right) 0.003 = 87 \left(1 - \frac{(2.5 \text{ in.})}{(3.604 \text{ in.})} \right) \\ &= 26.66 \text{ ksi} \end{aligned}$$

Use an iterative technique to find f'_s

Example: Doubly Reinforced Section

Compute the iterative values (2)

$$c = \frac{A_s f_y - A'_s f'_s}{0.85 f_c \beta_1 b} = \frac{(2.4 \text{ in}^2)(60 \text{ ksi}) - (0.62 \text{ in}^2)(30.66 \text{ ksi})}{0.85(4 \text{ ksi})(0.85)(12 \text{ in.})}$$

$$c = 3.676 \text{ in.}$$

$$\begin{aligned} f'_s &= E_s \varepsilon'_s = 29 \times 10^6 \left(1 - \frac{d'}{c} \right) 0.003 = 87 \left(1 - \frac{(2.5 \text{ in.})}{(3.676 \text{ in.})} \right) \\ &= 27.82 \text{ ksi} \end{aligned}$$

Use an iterative technique to find f'_s

Example: Doubly Reinforced Section

Compute the iterative values (etc)

$$c = \frac{A_s f_y - A'_s f'_s}{0.85 f_c \beta_1 b} = \frac{(2.4 \text{ in}^2)(60 \text{ ksi}) - (0.62 \text{ in}^2)(27.49 \text{ ksi})}{0.85(4 \text{ ksi})(0.85)(12 \text{ in.})}$$

$$c = 3.66 \text{ in.}$$

$$\begin{aligned} f'_s &= E_s \varepsilon'_s = 29 \times 10^6 \left(1 - \frac{d'}{c} \right) 0.003 = 87 \left(1 - \frac{(2.5 \text{ in.})}{(3.66 \text{ in.})} \right) \\ &= 27.57 \text{ ksi} \end{aligned}$$

Use $f'_s = 27.56 \text{ ksi}$ $c = 3.66 \text{ in}$

Example: Doubly Reinforced Section

Compute the moment capacity of the beam

$$\begin{aligned} M_n &= \left(A_s f_y - A'_s f'_s \right) \left(d - \frac{a}{2} \right) + A'_s f'_s (d - d') \\ &= \left((2.4 \text{ in}^2)(60 \text{ ksi}) - (0.62 \text{ in}^2)(27.56 \text{ ksi}) \right) \left(15.5 \text{ in.} - \frac{0.85(3.66 \text{ in.})}{2} \right) \\ &\quad + (0.62 \text{ in}^2)(27.56 \text{ ksi})(15.5 \text{ in.} - 2.5 \text{ in.}) \\ &= 1991.9 \text{ k-in.} \Rightarrow 166 \text{ k-ft} \end{aligned}$$