

boundary between inelastic and elastic columns, Equations 4.8 and 4.9 give the same value of F_{cr} . This occurs when KL/r is approximately

$$4.71 \sqrt{\frac{E}{F_y}}$$

To summarize,

$$\text{When } \frac{KL}{r} \leq 4.71 \sqrt{\frac{E}{F_y}}, \quad F_{cr} = (0.658^{F_y/F_e}) F_y \quad (4.10)$$

$$\text{When } \frac{KL}{r} > 4.71 \sqrt{\frac{E}{F_y}}, \quad F_{cr} = 0.877 F_e \quad (4.11)$$

The AISC Specification provides for separating inelastic and elastic behavior based on either the value of KL/r (as in equations 4.10 and 4.11) or the value of the ratio F_y/F_e . The limiting value of F_y/F_e can be derived as follows. From AISC Equation E3-4,

$$\frac{KL}{r} = \sqrt{\frac{\pi^2 E}{F_e}}$$

$$\text{For } \frac{KL}{r} \leq 4.71 \sqrt{\frac{E}{F_y}},$$

$$\sqrt{\frac{\pi^2 E}{F_e}} \leq 4.71 \sqrt{\frac{E}{F_y}}$$

$$\frac{F_y}{F_e} \leq 2.25$$

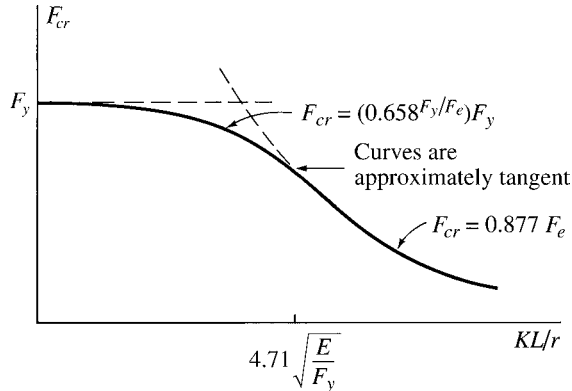
The complete AISC Specification for compressive strength is as follows:

$$\begin{aligned} \text{When } \frac{KL}{r} \leq 4.71 \sqrt{\frac{E}{F_y}} \quad \text{or} \quad \frac{F_y}{F_e} \leq 2.25, \\ F_{cr} = (0.658^{F_y/F_e}) F_y \end{aligned} \quad (\text{AISC Equation E3-2})$$

$$\begin{aligned} \text{When } \frac{KL}{r} > 4.71 \sqrt{\frac{E}{F_y}} \quad \text{or} \quad \frac{F_y}{F_e} > 2.25, \\ F_{cr} = 0.877 F_e \end{aligned} \quad (\text{AISC Equation E3-3})$$

In this book, we will usually use the limit on KL/r , as expressed in Equations 4.10 and 4.11. These requirements are represented graphically in Figure 4.8.

FIGURE 4.8



AISC Equations E3-2 and E3-3 are a condensed version of five equations that cover five ranges of KL/r (Galambos, 1988). These equations are based on experimental and theoretical studies that account for the effects of residual stresses and an initial out-of-straightness of $L/1500$, where L is the member length. A complete derivation of these equations is given by Tide (2001).

Although AISC does not require an upper limit on the slenderness ratio KL/r , an upper limit of 200 is recommended (see user note in AISC E2). This is a practical upper limit, because compression members that are any more slender will have little strength and will not be economical.

EXAMPLE 4.2

A $W14 \times 74$ of A992 steel has a length of 20 feet and pinned ends. Compute the design compressive strength for LRFD and the allowable compressive strength for ASD.

SOLUTION Slenderness ratio:

$$\text{Maximum } \frac{KL}{r} = \frac{KL}{r_y} = \frac{1.0(20 \times 12)}{2.48} = 96.77 < 200 \quad (\text{OK})$$

$$4.71 \sqrt{\frac{E}{F_y}} = 4.71 \sqrt{\frac{29,000}{50}} = 113$$

Since $96.77 < 113$, use AISC Equation E3-2.

$$F_e = \frac{\pi^2 E}{(KL/r)^2} = \frac{\pi^2 (29,000)}{(96.77)^2} = 30.56 \text{ ksi}$$

$$F_{cr} = 0.658^{(F_y/F_e)} F_y = 0.658^{(50/30.56)} (50) = 25.21 \text{ ksi}$$