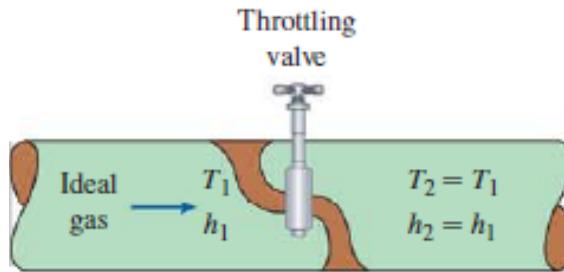


## Lecture nine

**8. Throttling process:** A process that takes place in such a way that the fluid expands through a \*minute aperture such as a narrow throat or a slightly opened valve in the line of flow, is known as *throttling process*. In this case, shaft work done,  $w_{1-2} = 0$ , adiabatically covered,  $q_{1-2} = 0$ . Changes in K.E. = 0 and P.E. = 0. Applying SFEE for single stream and 1 for inlet and 2 for exit.

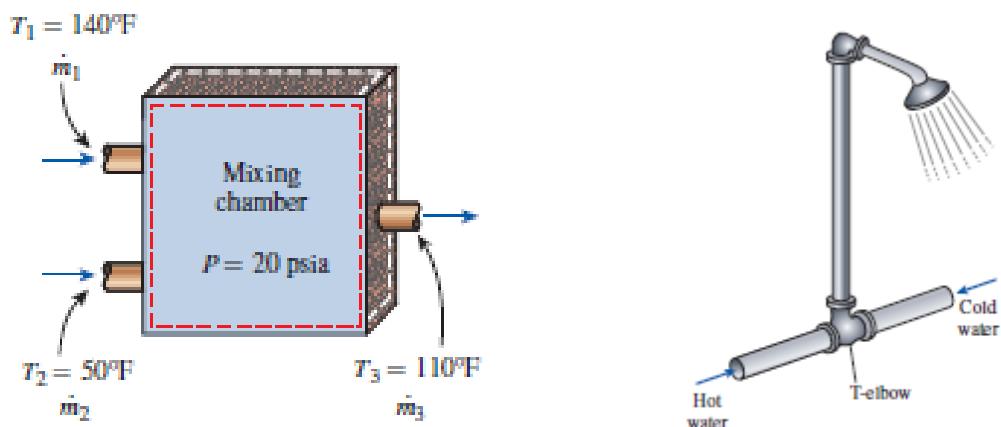
$$q_{1-2} - w_{1-2} = (h_2 + gz_2 + \frac{1}{2}V_2^2) - (h_1 + gz_1 + \frac{1}{2}V_1^2)$$

$m_1 = m_2, \quad h_1 = h_2 \quad \text{so, } T_1 = T_2 \text{ 'for gases only'}$



### 9. Mixing chamber:

Combining the mass and energy balances,



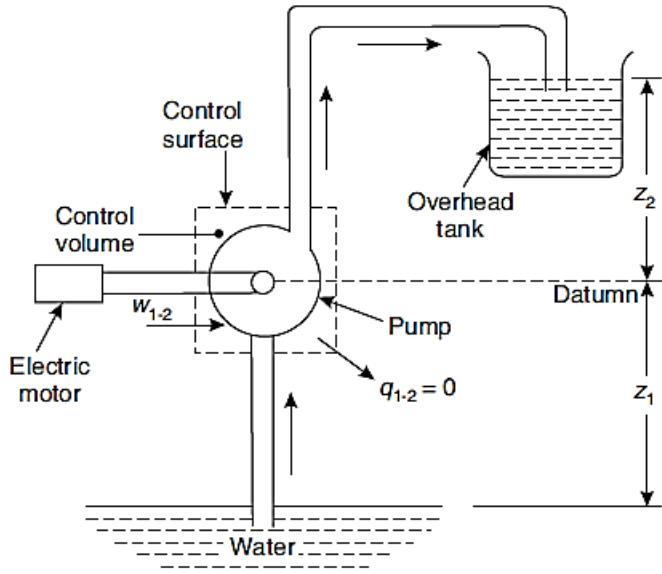
$$w_{1-2}=0, \quad PE=0, \quad KE=0, \quad q_{1-2}=0$$

$$m_1 h_1 + m_2 h_2 = (m_1 + m_2) h_3$$

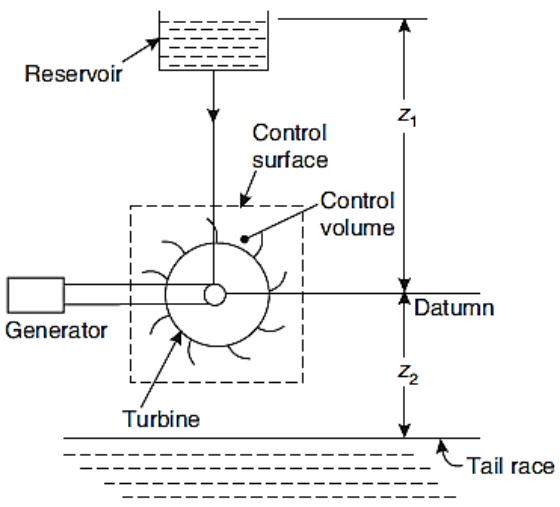
## 10. Centrifugal pump.

$$q_{1-2}=0, \quad u_1=u_2$$

$$-gz_1 + \frac{1}{2}V_1^2 + p_1 v_{s1} = gz_2 + \frac{1}{2}V_2^2 + p_1 v_{s2} - w_{1-2}$$



## 11. Water turbine.



$$gz_1 + \frac{1}{2}V_1^2 + p_1 v_{s1} = -gz_2 + \frac{1}{2}V_2^2 + p_1 v_{s2} + w_{1-2}$$



**Example 2//** A perfect gas flows through a nozzle where it expands in a reversible adiabatic manner. The inlet conditions are 22 bar, 500°C and 38 m/s. At exit, the pressure is 2 bar. Determine the exit temperature and velocity, if the flow rate is 4 kg / s. Take R = 190 J/kg. K and  $\gamma = 1.35$ .

**Solution.**

Inlet	Outlet (exit)
$p_1 = 22 \text{ bar} = 2200 \times 10^3 \text{ N/m}^2$	$p_2 = 2 \text{ bar} = 200 \times 10^3 \text{ N/m}^2$
$T_1 = 500^\circ\text{C} = 500 + 273 = 773 \text{ K}$	$T_2 = ?$
$V_1 = 38 \text{ m / s}$	$V_2 = ?$

Mass,  $m = 4 \text{ kg / s}$ , Gas constant,  $R = 190 \text{ J/kg K}$  and  $\gamma = 1.35$

We know that for a reversible adiabatic process:

$$\frac{T_2}{T_1} = \left[ \frac{P_2}{P_1} \right]^{\frac{\gamma-1}{\gamma}} = \left[ \frac{2}{22} \right]^{\frac{1.35-1}{1.35}} = \left( \frac{1}{11} \right)^{0.259} = 0.537$$

$$T_2 = T_1 \times 0.537 = 773 \times 0.537 = 415.1 \text{ K}$$

and change in enthalpy from inlet to exit,

$$h_1 - h_2 = cp (T_1 - T_2) = \frac{R \cdot \gamma}{\gamma - 1} = 190 \times \left[ \frac{1.35}{1.35 - 1} \right] \times (773 - 415.1) =$$

$$262.3 \times 10^3 \text{ J / kg}$$

Using the steady flow energy equation, we have

$$V_2 = \sqrt{V_1^2 + 2(h_1 - h_2)} = \sqrt{(38)^2 + 2(262.3 \times 10^3)} = 725.3 \text{ m/s}$$

**NOTE:**

We know that  $C_p - C_v = R$

$$\text{or } \frac{C_p - C_v}{C_v} = \frac{R}{C_v}$$

$$\text{or } \gamma - 1 = \frac{R}{C_v}$$

Multiply by  $C_p$  on both sides,

$$C_p(\gamma - 1) = \frac{R}{C_v} \times C_p = R \times \gamma \quad \text{or } C_p = \frac{R \times \gamma}{\gamma - 1}$$



**Example 3//** In a gas turbine, the gas enters at the rate of 5 kg / s with a velocity of 50 m / s and enthalpy of 900 kJ / kg and leaves the turbine with a velocity of 150 m/s and enthalpy of 400 kJ / kg. The loss of heat from the gases to the surroundings is 25 kJ / kg. Assume for gas,  $R = 0.285 \text{ kJ / kg K}$  and  $cp = 1.004 \text{ kJ/kg K}$ . The inlet condition is at 100 kPa and 27°C. Determine the power output of the turbine.

**Solution.**

Inlet	Exit
$V_1 = 50 \text{ m / s}$	$V_2 = 150 \text{ m / s}$
$h_1 = 900 \text{ kJ / kg}$	$h_2 = 400 \text{ kJ / kg}$
$p_1 = 100 \text{ kPa}$	
$T_1 = 27^\circ\text{C} = 27 + 273 = 300 \text{ K}$	

Mass of the gas  $m = 5 \text{ kg / s}$

Loss of heat to the surrounding,  $q_{1-2} = -25 \text{ kJ / kg}$  (– sign due to loss of heat)

Gas constant,  $R = 0.285 \text{ kJ / kg K}$ ,  $cp = 1.004 \text{ kJ / kg K}$

Now;

Let  $w_{1-2}$  = Work done or power output of the turbine.

Using the steady flow energy equation for a unit mass, we have

$$h_1 + gz_1 + \frac{1}{2}V_1^2 + q_{1-2} = h_2 + gz_2 + \frac{1}{2}V_2^2 + w_{1-2}$$

$$z_1 = z_2$$

$$h_1 + \frac{1}{2}V_1^2 + q_{1-2} = h_2 + \frac{1}{2}V_2^2 + w_{1-2}$$

$$900 + \frac{50^2}{2 \times 1000} + (-25) = 400 + \frac{150^2}{2 \times 1000} + w_{1-2}$$

$$1.25 + 900 - 25 = 11.25 + 400 + w_{1-2}$$

$$876.25 = 411.25 + w_{1-2}$$

$$w_{1-2} = 876.25 - 411.25 = 465 \text{ kJ/kg}$$

Since the mass of gas is 5 kg / s; therefore, power output of the turbine,

$$W_{1-2} = 5 \times 465 = 2325 \text{ kJ/s} = 2325 \text{ kW} \quad \text{Ans....( } 1 \text{ kJ/s} = 1 \text{ kW})$$



**Example 4//** Air at a temperature of 20°C passes through a heat exchanger at a velocity of 40 m / s, where its temperature is raised to 820°C. It then enters a turbine with the same velocity of 40 m/s and expands till the temperature falls to 620°C. On leaving the turbine, the air is taken at a velocity of 55 m / s to a nozzle where it expands until the temperature has fallen to 510°C. If the air flow rate is 2.5 kg / s; calculate:

1. Rate of heat transfer to the air in the heat exchanger.
2. The power output from the turbine, assuming no heat loss; and
3. The velocity at exit from the nozzle, assuming no heat loss.

Take enthalpy of air as  $h = cp dT$ , where  $cp$  is the specific heat at constant pressure and taken as 1.005 kJ / kg K and  $dT = T_2 - T_1$ , is the change in temperature.

**Solution.**

Given: Temperature of air entering the heat exchanger,

$$T_1 = 20^\circ\text{C} = 20 + 273 = 293 \text{ K}$$

Velocity of air,  $V_1 = 40 \text{ m / s}$

Temperature of air leaving the heat exchanger,

$$T_2 = 820^\circ\text{C} = 820 + 273 = 1093 \text{ K}$$

Velocity of air entering the turbine,

$$V_2 = V_1 = 40 \text{ m / s}$$

Temperature of air leaving the turbine,

$$T_3 = 620^\circ\text{C} = 620 + 273 = 893 \text{ K}$$

Velocity of air leaving the turbine or entering the nozzle,

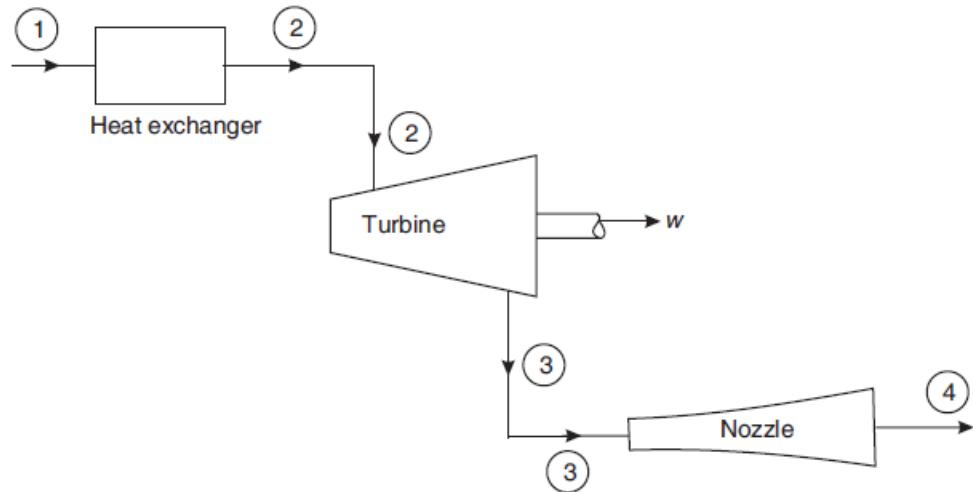
$$V_3 = 55 \text{ m / s}$$

Temperature of air leaving the nozzle,

$$T_4 = 510^\circ\text{C} = 510 + 273 = 783 \text{ K}$$

Air flow rate,  $m = 2.5 \text{ kg / s}$ .

## 1. Rate of heat transfer to the air in the heat exchanger



First of all, let us consider heat transfer through a heat exchanger.

Applying the steady flow energy equation, we have

$$h_1 + gz_1 + \frac{1}{2}V_1^2 + q_{1-2} = h_2 + gz_2 + \frac{1}{2}V_2^2 + w_{1-2}$$

$z_1 = z_2$ ,  $V_2 = V_1$  and  $w_{1-2} = 0$ , for a heat exchanger, therefore,

$$q_{1-2} = h_2 - h_1 = c_p (T_2 - T_1) = 1.005 (1093 - 293) = 804 \text{ kJ/kg}$$

Since the air flow rate ( $m$ ) is 2.5 kg / s, therefore rate of heat transfer,

$$Q_{1-2} = m \times q_{1-2} = 2.5 \times 804 = 2010 \text{ kJ / s or kW} \dots (1 \text{ kJ / s} = 1 \text{ kW})$$

## 2. Power output from the turbine

Let  $W_{1-2}$  = Work done or power output from the turbine in kW.

Applying the steady flow energy equation, we have

$$h_2 + gz_2 + \frac{1}{2}V_2^2 + q_{2-3} = h_3 + gz_3 + \frac{1}{2}V_3^2 + w_{2-3}$$

$$z_2 = z_3 \text{ and } q_{2-3} = 0$$

$$h_2 + \frac{1}{2}V_2^2 = h_3 + \frac{1}{2}V_3^2 + w_{2-3}$$

$$w_{2-3} = \left( \frac{V_2^2 - V_3^2}{2 \times 1000} \right) + (h_2 - h_3) = \left( \frac{V_2^2 - V_3^2}{2 \times 1000} \right) + cp (T_2 - T_3)$$

$$= \left[ \frac{40^2 - 55^2}{2 \times 1000} \right] + 1.005 (1093 - 893) = -0.7125 + 201 = 200.2875 \text{ kJ / kg}$$



Since the air flow rate ( $m$ ) is 2.5 kg / s, therefore power output from the turbine.

$$W_{1-2} = m \times w_{1-2} = 2.5 \times 200.2875 = 500.72 \text{ kJ / s or kW}$$

3. Velocity at exit from the nozzle

Let  $V_4$  = Velocity at exit from the nozzle in m / s.

$$h_3 + gz_3 + \frac{1}{2}V_3^2 + q_{3-4} = h_4 + gz_4 + \frac{1}{2}V_4^2 + w_{3-4}$$

$$z_3 = z_4, q_{3-4} = 0, \text{ and } w_{3-4} = 0$$

$$h_3 + \frac{1}{2}V_3^2 = h_4 + \frac{1}{2}V_4^2$$

$$V_4 = \sqrt{V_3^2 + 2(h_3 - h_4)} = \sqrt{V_3^2 + 2c_p(T_3 - T_4)} = \sqrt{(55)^2 + 2 \times 1.005(893 - 783)} \\ = 473.43 \text{ m/s}$$



## ASSIGNMENTS

1. In a steam plant, 1 kg of water per second is supplied to the boiler. The enthalpy and velocity of water entering the boiler are 800 kJ / kg and 5 m / s. The water receives 2200 kJ / kg of heat in the boiler at constant pressure. The steam after passing through the turbine comes out with a velocity of 50 m / s and its enthalpy is 2520 kJ / kg. The inlet is 4 m above the turbine exit. The heat losses from the boiler and turbine to the surroundings are 20 kJ / s. Calculate the power developed by the turbine considering boiler and turbine as single system.
2. In a water turbine, the water head measured from the center of the turbine is 1500 m and the flow rate is 500 kg / s. The tail race is 3 m below the turbine center line and outlet velocity is 10 m / s. Determine the power developed by the turbine.
3. Air enters an air compressor at 8 m/s velocity, 100 kPa pressure and 0.95 m<sup>3</sup>/ kg volume. It flows steadily at the rate of 0.6 kg / s and leaves at 6 m/s, 700 kPa and 0.19 m<sup>3</sup>/ kg. The internal energy of the air leaving is 90 kJ / kg greater than that of air entering. The cooling water in the compressor jackets absorbs heat from the air at the rate of 60 kW. Find: 1. The ratio of the inlet pipe diameter to outlet pipe diameter; and 2. The rate of shaft work input to the air in kW.
4. A centrifugal pump delivers water at the rate of 45.5 kg/s by increasing the pressure from 80 kN/m<sup>2</sup> to 280 kN/m<sup>2</sup>. The suction is 2 m below the centre of the pump and delivery is 5 m above the center of the pump. The suction and delivery pipe diameters are 150 mm and 100 mm respectively. Determine the power required to drive the pump.